



(12) **United States Patent**  
**Takahashi et al.**

(10) **Patent No.:** **US 9,085,299 B2**  
(45) **Date of Patent:** **Jul. 21, 2015**

- (54) **DRIVE CONTROL DEVICE FOR HYBRID VEHICLE**
- (75) Inventors: **Satoru Takahashi**, Nagoya (JP); **Tomoyuki Maruyama**, Tajimi (JP); **Hiroaki Kiyokami**, Toyota (JP); **Satoshi Kasamai**, Miyoshi (JP); **Koki Ueno**, Susono (JP); **Takeshi Miyagawa**, Toyokawa (JP); **Norihiro Yamamura**, Miyoshi (JP); **Yoshitaka Suzuki**, Aichi-gun (JP); **Hiroki Kuwamoto**, Toyota (JP); **Tomohito Ono**, Gotenba (JP)
- (73) Assignee: **TOYOTA JIDOSHA KABUSHIKI KAISHA**, Aichi-ken (JP)
- (\* ) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

- (21) Appl. No.: **14/386,208**
- (22) PCT Filed: **Mar. 21, 2012**
- (86) PCT No.: **PCT/JP2012/057156**

§ 371 (c)(1),  
(2), (4) Date: **Sep. 18, 2014**

- (87) PCT Pub. No.: **WO2013/140543**  
PCT Pub. Date: **Sep. 26, 2013**

- (65) **Prior Publication Data**  
US 2015/0073635 A1 Mar. 12, 2015

- (51) **Int. Cl.**  
**B60W 20/00** (2006.01)  
**B60K 6/445** (2007.10)  
**B60W 10/08** (2006.01)  
**B60K 6/48** (2007.10)  
**B60W 10/02** (2006.01)  
**B60W 10/12** (2012.01)  
**B60W 10/196** (2012.01)  
**B60K 6/38** (2007.10)

- (52) **U.S. Cl.**  
CPC ..... **B60W 20/40** (2013.01); **B60K 6/445** (2013.01); **B60K 6/48** (2013.01); **B60W 10/02** (2013.01);

- (58) **Field of Classification Search**  
CPC ..... B60W 10/00; B60W 10/04; B60W 10/06; B60W 10/08; B60W 10/18; B60W 20/00; B60W 20/10; B60W 20/40; B60K 6/42; B60K 6/46  
USPC ..... 701/22; 180/65.1, 65.21, 65.265, 180/65.285; 903/902, 911, 930  
See application file for complete search history.

- (56) **References Cited**  
**U.S. PATENT DOCUMENTS**  
6,478,705 B1 \* 11/2002 Holmes et al. .... 475/5  
8,313,401 B2 \* 11/2012 Kim et al. .... 475/5

(Continued)

**FOREIGN PATENT DOCUMENTS**

- EP 2 058 160 A1 5/2009
- JP 4038183 B2 1/2008

(Continued)

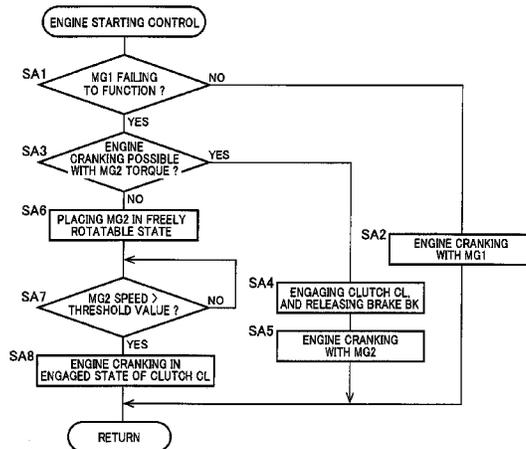
*Primary Examiner* — Thomas Tarcza  
*Assistant Examiner* — Tyler J Lee  
(74) *Attorney, Agent, or Firm* — Sughrue Mion, PLLC

(57) **ABSTRACT**

A drive control device for a hybrid vehicle is provided with a differential device including four rotary elements; and an engine, first and second electric motors and an output rotary member which are respectively connected to the four rotary elements. One of the four rotary elements is constituted by a rotary component of a first differential mechanism and a rotary component of a second differential mechanism selectively connected through a clutch, and one of the rotary components of the first and second differential mechanisms which are selectively connected to each other through the clutch is selectively fixed to a stationary member through a brake. The drive control device comprises: an electric motor operation control portion configured to control the second electric motor for starting the engine with an output torque of the second electric motor, when a reaction force is exerted on the first and second electric motors.

(Continued)

**6 Claims, 11 Drawing Sheets**



(52) **U.S. Cl.**

CPC ..... **B60W 10/08** (2013.01); **B60W 10/12**  
 (2013.01); **B60W 10/196** (2013.01); **B60W**  
**20/50** (2013.01); **B60K 2006/381** (2013.01);  
**B60W 2710/06** (2013.01); **B60W 2710/083**  
 (2013.01); **Y02T 10/6221** (2013.01); **Y02T**  
**10/6239** (2013.01); **Y10S 903/93** (2013.01)

2008/0053723	A1 *	3/2008	Kozarekar .....	180/65.2
2008/0275624	A1	11/2008	Snyder	
2010/0116235	A1	5/2010	Imamura et al.	
2011/0111906	A1 *	5/2011	Kim et al. ....	475/5
2013/0006459	A1 *	1/2013	Kim et al. ....	701/22
2014/0174856	A1 *	6/2014	Takagi et al. ....	184/6.12
2014/0194238	A1	7/2014	Ono et al.	
2014/0194239	A1 *	7/2014	Ono et al. ....	475/5
2015/0031487	A1 *	1/2015	Kiyokami et al. ....	475/5

(56)

**References Cited**

U.S. PATENT DOCUMENTS

8,597,147	B2 *	12/2013	Kim et al. ....	475/5
2004/0121870	A1 *	6/2004	Takenaka et al. ....	475/5

FOREIGN PATENT DOCUMENTS

JP	2008-265600	A	11/2008
WO	2013/014777	A1	1/2013

\* cited by examiner

FIG. 1

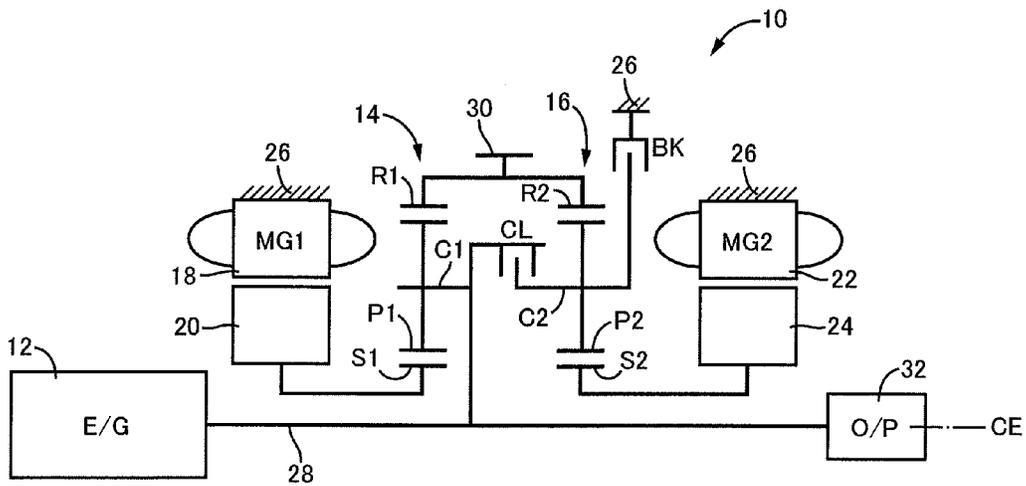


FIG. 2

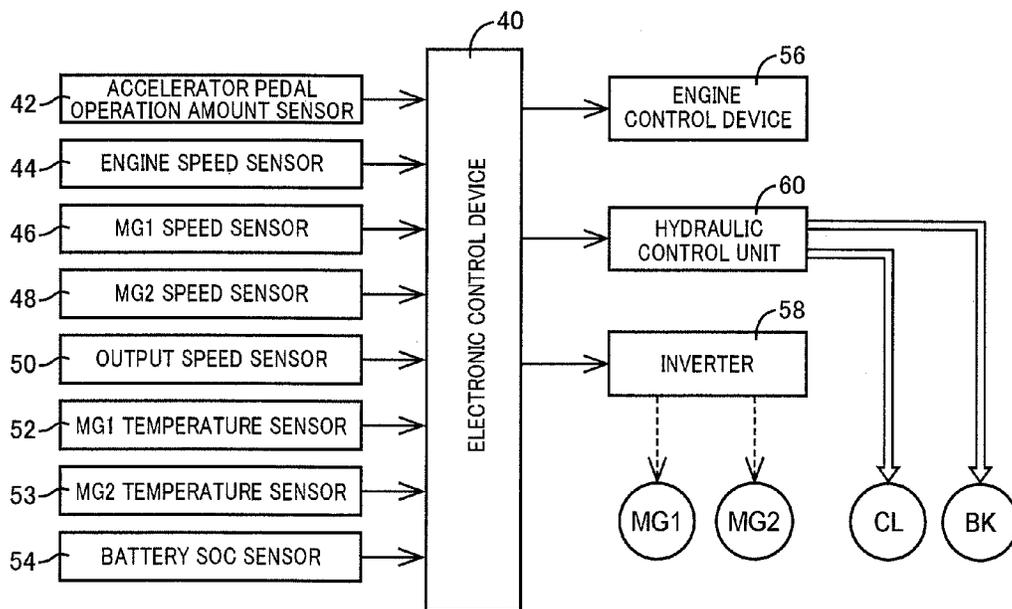


FIG.3

	BK	CL	MODE
EV-1	○		1
EV-2	○	○	2
HV-1	○		3
HV-2		○	4
HV-3			5

FIG.4

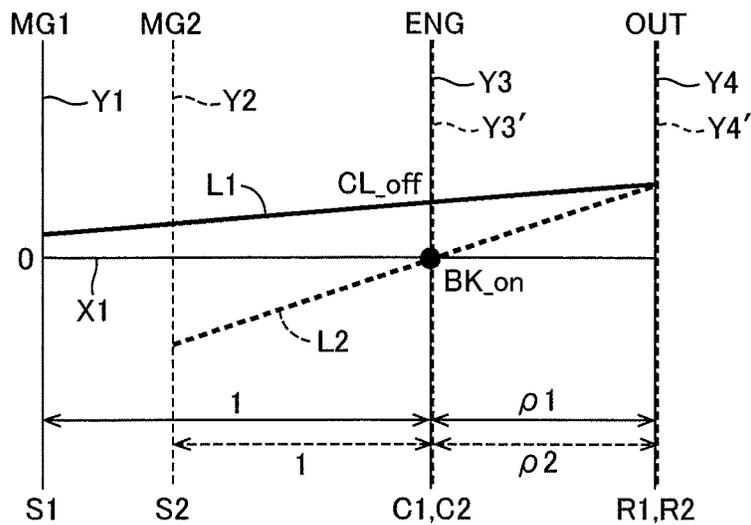


FIG.5

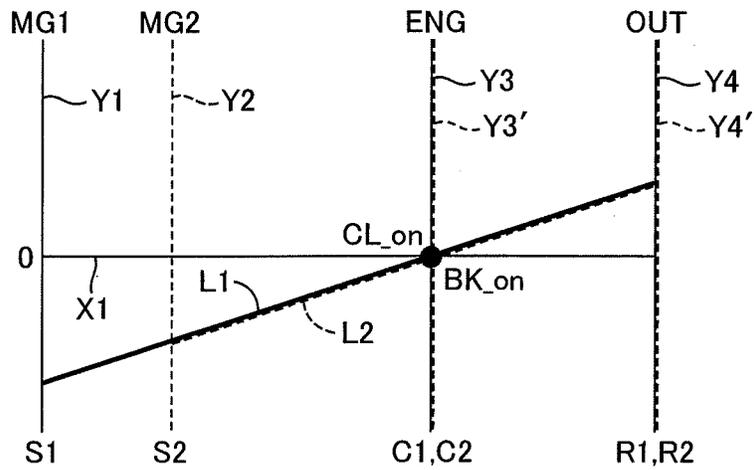


FIG.6

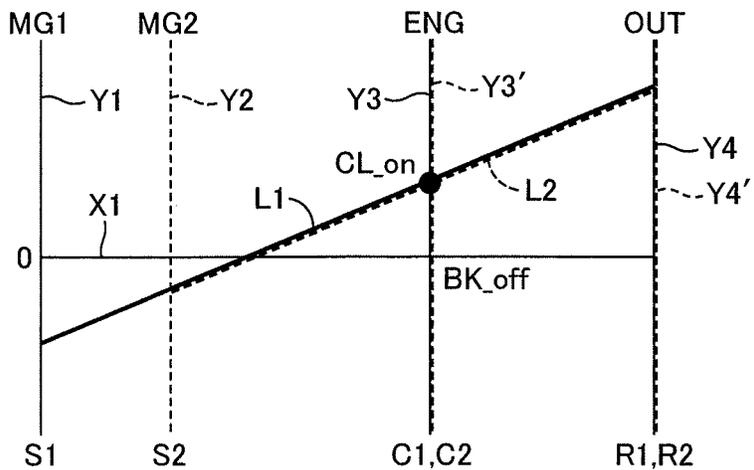


FIG. 7

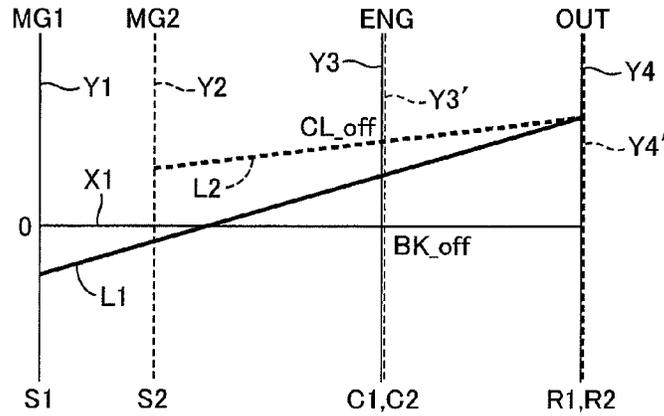


FIG. 8

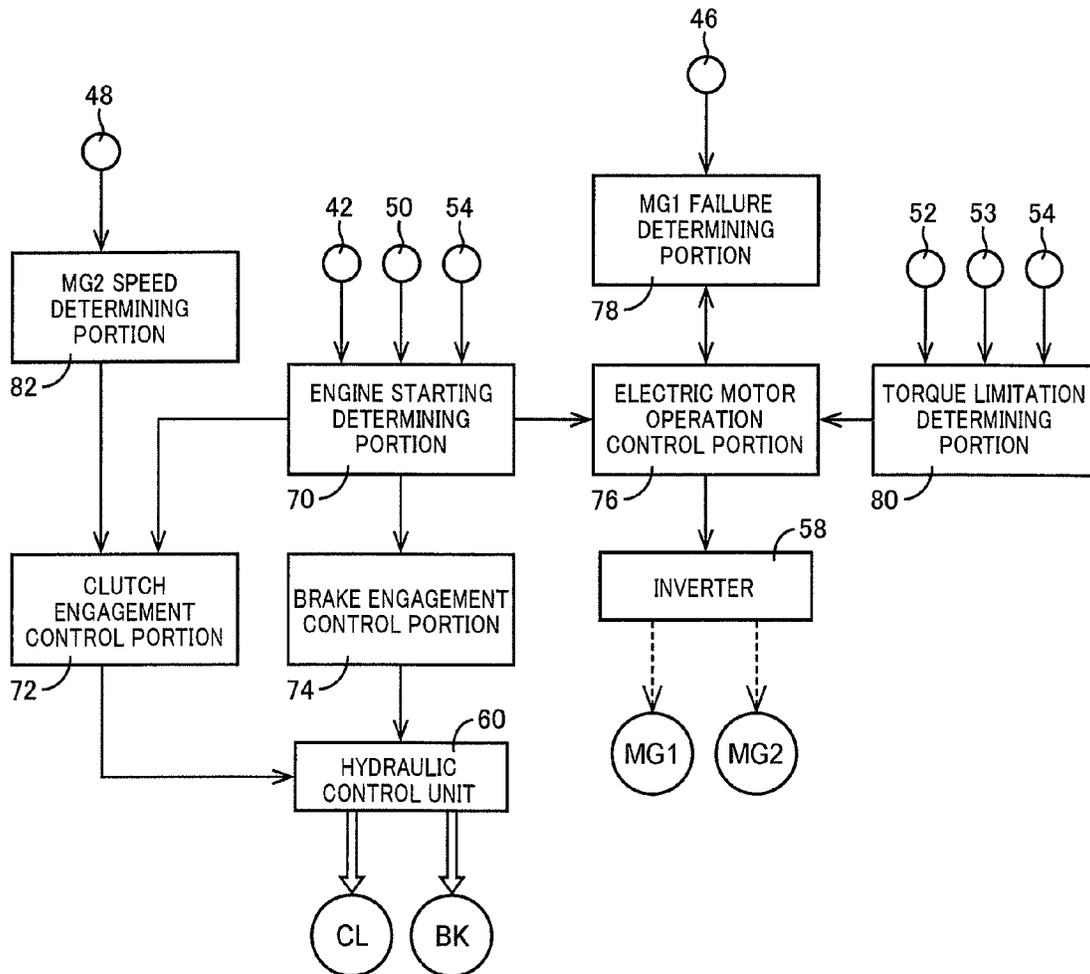


FIG.9

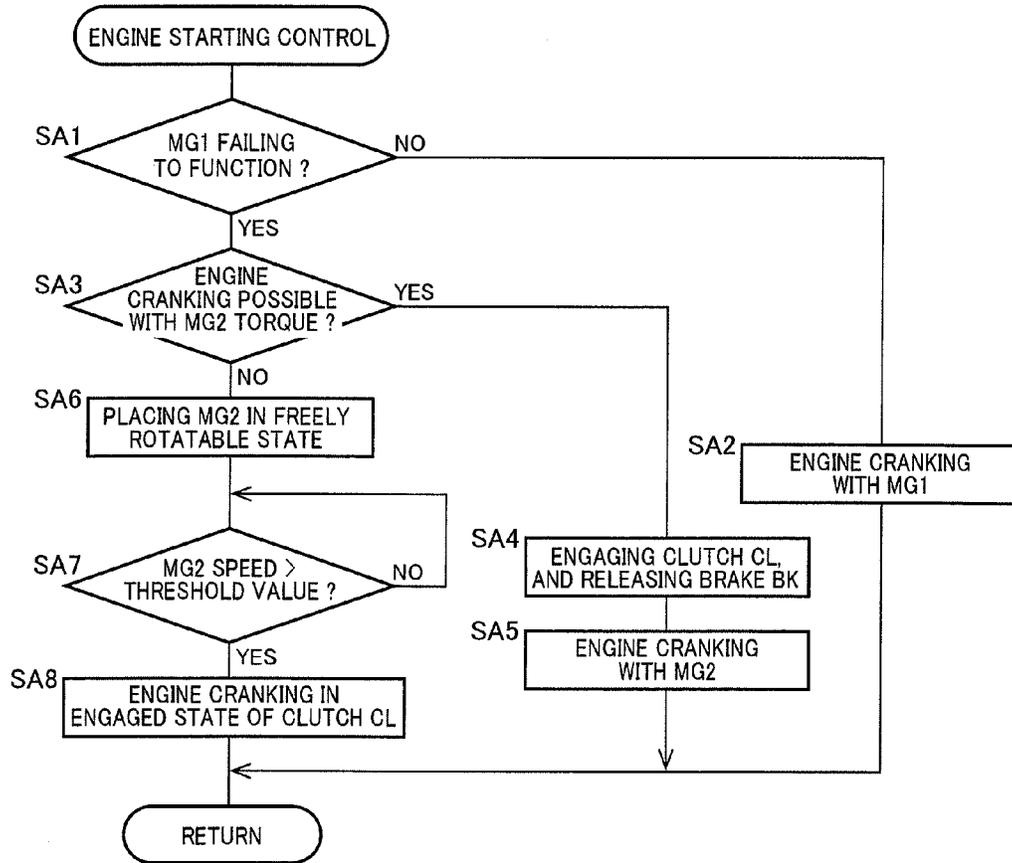


FIG.10

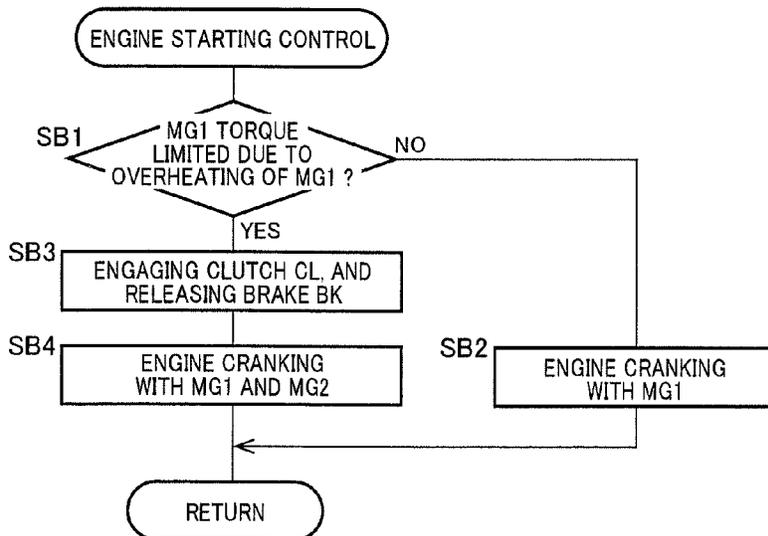


FIG.11

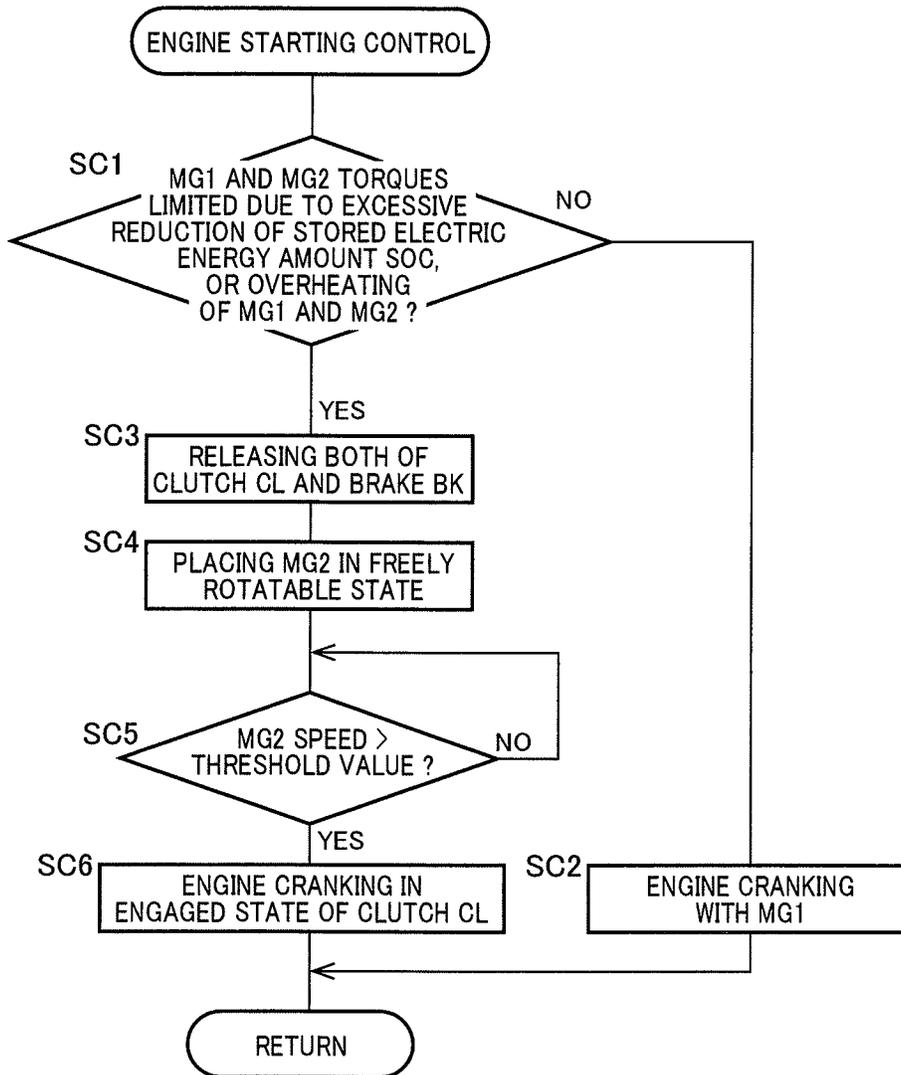


FIG.12

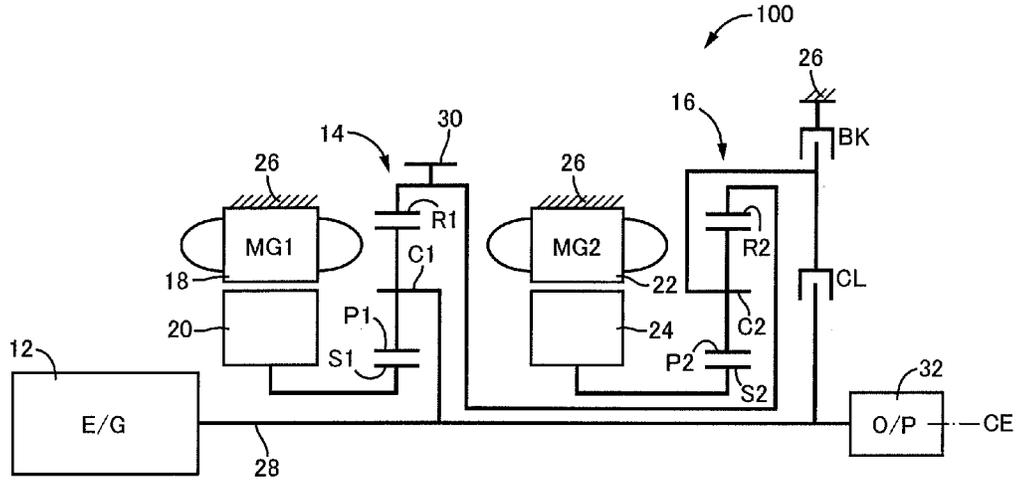


FIG.13

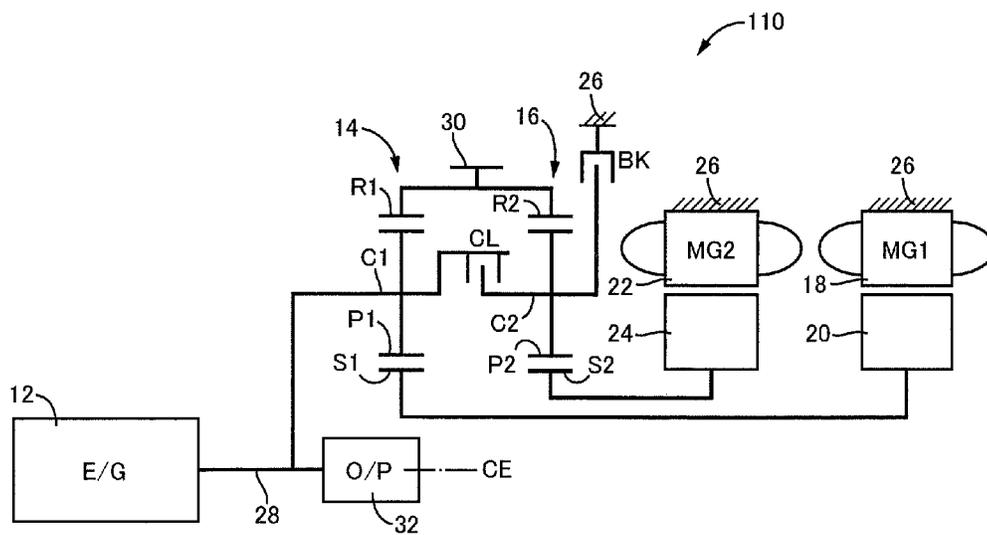


FIG. 14

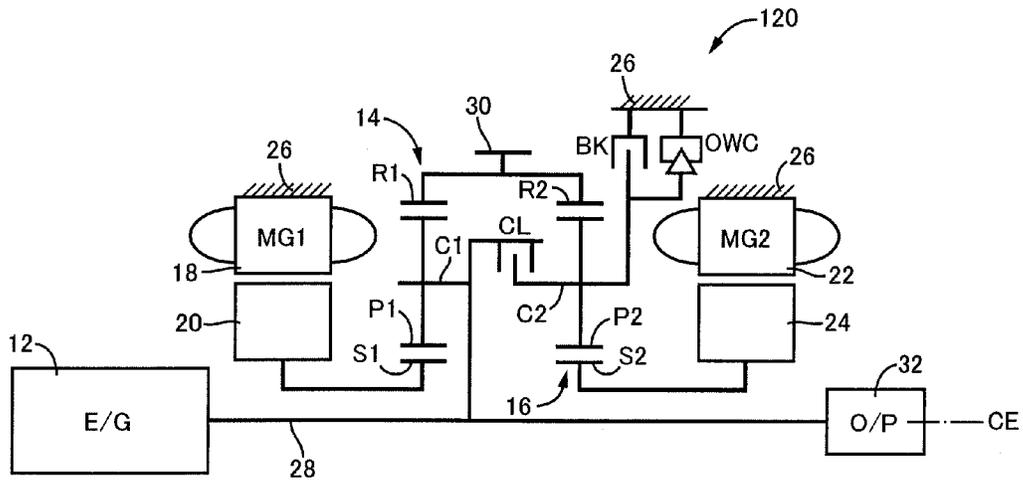


FIG. 15

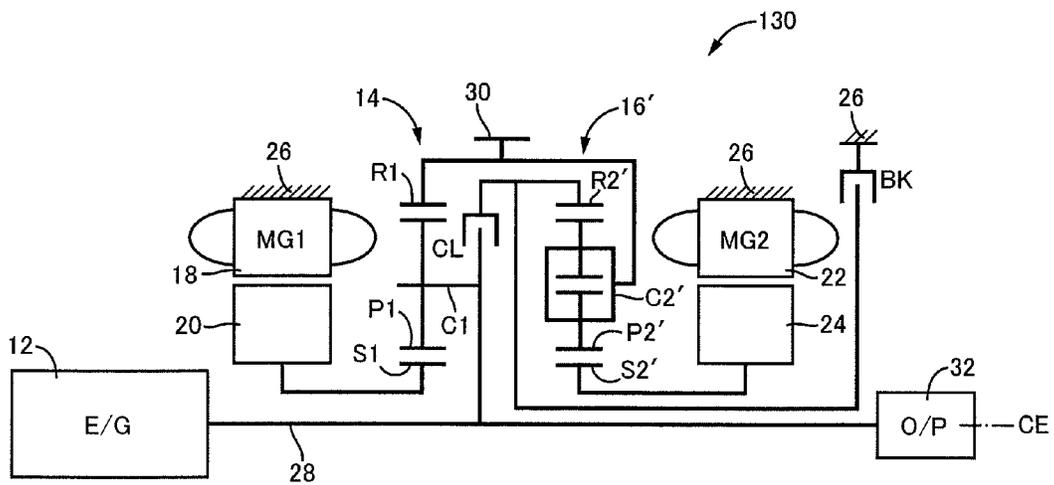




FIG.18

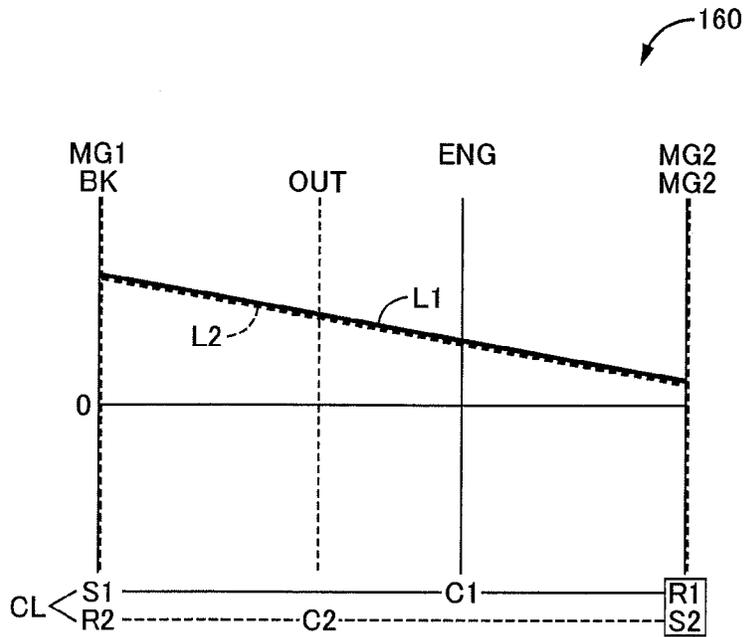


FIG.19

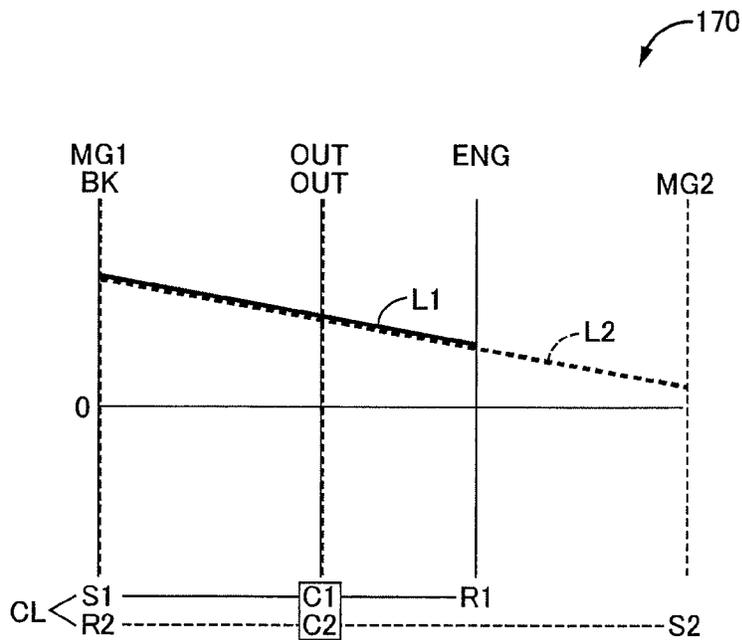
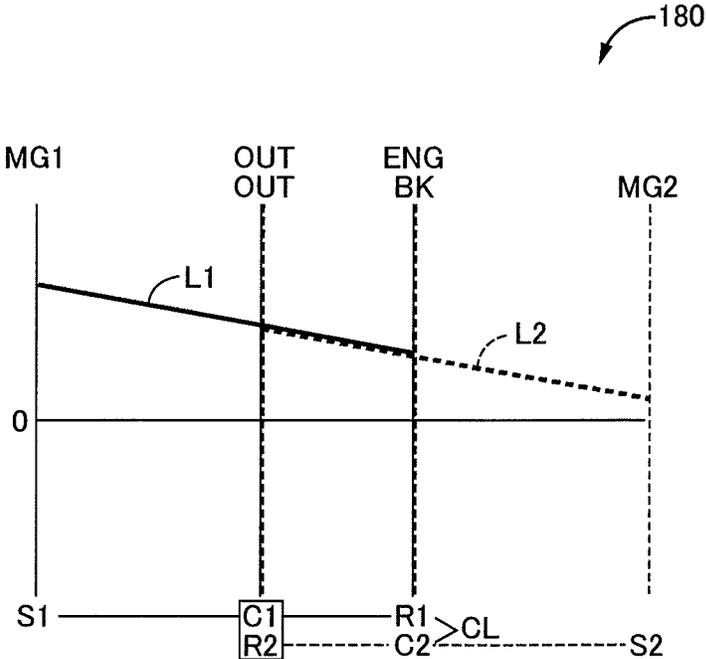


FIG.20



1

**DRIVE CONTROL DEVICE FOR HYBRID  
VEHICLE****CROSS REFERENCE TO RELATED  
APPLICATIONS**

This application is a National Stage of International Application No. PCT/JP2012/057156, Mar. 21, 2012, the contents of all of which are incorporated herein by reference in their entirety.

**TECHNICAL FIELD**

The present invention relates to an improvement of a drive control device for a hybrid vehicle.

**BACKGROUND ART**

There is known a hybrid vehicle which has at least one electric motor in addition to an engine such as an internal combustion engine, which functions as a vehicle drive power source. Patent Document 1 discloses an example of such a hybrid vehicle, which is provided with an internal combustion engine, a first electric motor and a second electric motor. This hybrid vehicle is further provided with a brake which is configured to fix an output shaft of the above-described internal combustion engine to a stationary member, and an operating state of which is controlled according to a running condition of the hybrid vehicle, so as to improve energy efficiency of the hybrid vehicle and to permit the hybrid vehicle to run according to a requirement by an operator of the hybrid vehicle.

**PRIOR ART DOCUMENT**

## Patent Document

Patent Document 1: JP-2008-265600 A1

Patent Document 2: JP-4038183 B2

**SUMMARY OF THE INVENTION**

## Object Achieved by the Invention

According to the conventional arrangement of the hybrid vehicle described above, however, the engine which has been held at rest cannot be adequately started. In the event of a failure of the first electric motor, for example, the engine cannot be cranked by the first electric motor, and cannot be started. Where the first electric motor cannot generate a sufficient output torque due to excessive reduction of an electric energy amount SOC stored in a battery, for instance, the engine cannot be started with a high degree of stability. These problems were first discovered by the present inventors in the process of intensive studies in an attempt to improve the performance of the hybrid vehicle.

The present invention was made in view of the background art described above. It is therefore an object of the present invention to provide a drive control device for a hybrid vehicle, which permits adequate starting of an engine.

## Means for Achieving the Object

The object indicated above is achieved according to a first aspect of the present invention, which provides a drive control device for a hybrid vehicle provided with: a first differential mechanism and a second differential mechanism which have four rotary elements as a whole; and an engine, a first electric

2

motor, a second electric motor and an output rotary member which are respectively connected to the above-described four rotary elements, and wherein one of the above-described four rotary elements is constituted by the rotary element of the above-described first differential mechanism and the rotary element of the above-described second differential mechanism which are selectively connected to each other through a clutch, and one of the rotary elements of the above-described first and second differential mechanisms which are selectively connected to each other through the above-described clutch is selectively fixed to a stationary member through a brake, the drive control device being characterized by starting the above-described engine with an output torque of the above-described second electric motor, when a reaction force is exerted on the above-described first and second electric motors.

## Advantages of the Invention

According to the first aspect of the invention described above, the hybrid vehicle is provided with: the first differential mechanism and the second differential mechanism which have the four rotary elements as a whole; and the engine, the first electric motor, the second electric motor and the output rotary member which are respectively connected to the four rotary elements. One of the above-described four rotary elements is constituted by the rotary element of the above-described first differential mechanism and the rotary element of the above-described second differential mechanism which are selectively connected to each other through the clutch, and one of the rotary elements of the above-described first and second differential mechanisms which are selectively connected to each other through the clutch is selectively fixed to the stationary member through the brake. The drive control device is configured to start the above-described engine with the output torque of the above-described second electric motor, when a reaction force is exerted on the above-described first and second electric motors. Accordingly, the engine can be adequately started by cranking of the engine with the above-described second electric motor, even in the event of a failure of the above-described first electric motor. Namely, the present invention provides the drive control device for the hybrid vehicle, which permits adequate starting of the engine.

According to a second aspect of the invention, the drive control device according to the first aspect of the invention is configured to start the above-described engine with an output torque of at least one of the above-described first and second electric motors, in an engaged state of the above-described clutch and in a released state of the above-described brake. According to this second aspect of the invention, the engine is cranked with both of the above-described first and second electric motors, for example, so that a rotary motion speed of the engine can be rapidly raised through a resonance band of a power transmitting system, whereby a starting shock of the engine can be reduced.

According to a third aspect of the invention, the drive control device according to the first aspect of the invention is configured to start the above-described engine primarily with the output torque of the above-described second electric motor, in an engaged state of the above-described clutch and in a released state of the above-described brake, in the event of a failure of the above-described first electric motor. According to this third aspect of the invention, the above-described engine can be adequately started by cranking with the second electric motor, even in the event of a failure of the above-described first electric motor.

According to a fourth aspect of the invention, the drive control device according to the first aspect of the invention is configured to start the above-described engine by bringing the above-described clutch into an engaged state after a rise of a speed of the above-described second electric motor placed in a freely rotatable state, when either of the above-described first and second electric motors cannot generate a torque required to crank the above-described engine. According to this fourth aspect of the invention, the above-described engine can be adequately started by cranking the engine by the output torque of the above-described second electric motor having a rotary motion inertia, even where the output torque of the second electric motor should be limited due to excessive reduction of an electric energy amount stored in a battery.

According to a fifth aspect of the invention, the drive control device according to the fourth aspect of the invention is configured to start the above-described engine by bringing the above-described clutch into the engaged state after the rise of the speed of the above-described second electric motor to a predetermined value corresponding to an inertia force required to crank the above-described engine. According to this fifth aspect of the invention, it is possible to crank the engine in a highly practical manner for starting the engine, with the output torque of the above-described second electric motor having the rotary motion inertia.

According to a sixth aspect of the invention, the drive control device according to any one of the first, second, third, fourth and fifth aspects of the invention is configured such that the above-described first differential mechanism is provided with a first rotary element connected to the above-described first electric motor, a second rotary element connected to the above-described engine, and a third rotary element connected to the above-described output rotary member, while the above-described second differential mechanism is provided with a first rotary element connected to the above-described second electric motor, a second rotary element, and a third rotary element, one of the second and third rotary elements being connected to the third rotary element of the above-described first differential mechanism, and the above-described clutch is configured to selectively connect the second rotary element of the above-described first differential mechanism, and the other of the second and third rotary elements of the above-described second differential mechanism which is not connected to the third rotary element of the above-described first differential mechanism, to each other, while the above-described brake is configured to selectively fix the other of the second and third rotary elements of the above-described second differential mechanism which is not connected to the third rotary element of the above-described first differential mechanism, to the stationary member. According to this sixth aspect of the invention, the engine can be adequately started in a drive system of the hybrid vehicle, which has a highly practical arrangement.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic view for explaining an arrangement of a hybrid vehicle drive system to which the present invention is suitably applicable;

FIG. 2 is a view for explaining major portions of a control system provided to control the drive system of FIG. 1;

FIG. 3 is a table indicating combinations of operating states of a clutch and a brake, which correspond to respective five drive modes of the drive system of FIG. 1;

FIG. 4 is a collinear chart having straight lines which permit indication thereon of relative rotating speeds of vari-

ous rotary elements of the drive system of FIG. 1, the collinear chart corresponding to the modes 1 and 3 of FIG. 3;

FIG. 5 is a collinear chart having straight lines which permit indication thereon of relative rotating speeds of various rotary elements of the drive system of FIG. 1, the collinear chart corresponding to the mode 2 of FIG. 3;

FIG. 6 is a collinear chart having straight lines which permit indication thereon of relative rotating speeds of various rotary elements of the drive system of FIG. 1, the collinear chart corresponding to the mode 4 of FIG. 3;

FIG. 7 is a collinear chart having straight lines which permit indication thereon of relative rotating speeds of various rotary elements of the drive system of FIG. 1, the collinear chart corresponding to the mode 5 of FIG. 3;

FIG. 8 is a functional block diagram for explaining major control functions of an electronic control device of FIG. 2;

FIG. 9 is a flow chart for explaining a major portion of an example of an engine starting control implemented by the electronic control device of FIG. 2;

FIG. 10 is a flow chart for explaining a major portion of another example of the engine starting control implemented by the electronic control device of FIG. 2;

FIG. 11 is a flow chart for explaining a major portion of a further example of the engine starting control implemented by the electronic control device of FIG. 2;

FIG. 12 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to another preferred embodiment of this invention;

FIG. 13 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to a further preferred embodiment of this invention;

FIG. 14 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to a still further preferred embodiment of this invention;

FIG. 15 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to a yet further preferred embodiment of this invention;

FIG. 16 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to still another preferred embodiment of this invention;

FIG. 17 is a schematic view for explaining an arrangement of a hybrid vehicle drive system according to yet another preferred embodiment of this invention;

FIG. 18 is a collinear chart for explaining an arrangement and an operation of a hybrid vehicle drive system according to another preferred embodiment of this invention;

FIG. 19 is a collinear chart for explaining an arrangement and an operation of a hybrid vehicle drive system according to a further preferred embodiment of this invention; and

FIG. 20 is a collinear chart for explaining an arrangement and an operation of a hybrid vehicle drive system according to a still further preferred embodiment of this invention.

#### MODE FOR CARRYING OUT THE INVENTION

According to the present invention, the first and second differential mechanisms as a whole have four rotary elements while the above-described clutch is placed in the engaged state. In one preferred form of the present invention, the first and second differential mechanisms as a whole have four rotary elements while a plurality of clutches, each of which is provided between the rotary elements of the first and second differential mechanisms and which includes the above-described clutch, are placed in their engaged states. In other words, the present invention is suitably applicable to a drive control device for a hybrid vehicle which is provided with the first and second differential mechanisms represented as the

5

four rotary elements indicated in a collinear chart, the engine, the first electric motor, the second electric motor and the output rotary member coupled to the respective four rotary elements, and wherein one of the four rotary elements is selectively connected through the above-described clutch to another of the rotary elements of the first differential mechanism and another of the rotary elements of the second differential mechanism, while the rotary element of the first or second differential mechanism to be selectively connected to the above-indicated one rotary element through the clutch is selectively fixed through the above-described brake to the stationary member.

In another preferred form of the present invention, the above-described clutch and brake are hydraulically operated coupling devices operating states (engaged and released states) of which are controlled according to a hydraulic pressure. While wet multiple-disc type frictional coupling devices are preferably used as the clutch and brake, meshing type coupling devices, namely, so-called dog clutches (claw clutches) may also be used. Alternatively, the clutch and brake may be electromagnetic clutches, magnetic powder clutches and any other clutches the operating states of which are controlled (which are engaged and released) according to electric commands.

The drive system to which the present invention is applicable is placed in a selected one of a plurality of drive modes, depending upon the operating states of the above-described clutch and brake. Preferably, EV drive modes in which at least one of the above-described first and second electric motors is used as a vehicle drive power source with the engine stopped include a mode 1 to be established in the engaged state of the brake and in the released state of the clutch, and a mode 2 to be established in the engaged states of both of the clutch and brake. Further, hybrid drive modes in which the above-described engine is operated while the above-described first and second electric motors are operated to generate a vehicle drive force and/or an electric energy as needed, include a mode 3 to be established in the engaged state of the brake and in the released state of the clutch, a mode 4 to be established in the released state of the brake and the engaged state of the clutch, and a mode 5 to be established in the released states of both of the brake and clutch.

In a further preferred form of the invention, the rotary elements of the above-described first differential mechanism, and the rotary elements of the above-described second differential mechanism are arranged as seen in the collinear charts, in the engaged state of the above-described clutch and in the released state of the above-described brake, in the order of the first rotary element of the first differential mechanism, the first rotary element of the second differential mechanism, the second rotary element of the first differential mechanism, the second rotary element of the second differential mechanism, the third rotary element of the first differential mechanism, and the third rotary element of the second differential mechanism, where the rotating speeds of the second rotary elements and the third rotary elements of the first and second differential mechanisms are indicated in mutually overlapping states in the collinear charts.

Referring to the drawings, preferred embodiments of the present invention will be described in detail. It is to be understood that the drawings referred to below do not necessarily accurately represent ratios of dimensions of various elements. First Embodiment

FIG. 1 is the schematic view for explaining an arrangement of a hybrid vehicle drive system 10 (hereinafter referred to simply as a "drive system 10") to which the present invention is suitably applicable. As shown in FIG. 1, the drive system 10

6

according to the present embodiment is of a transversely installed type suitably used for an FF (front-engine front-drive) type vehicle, and is provided with a main vehicle drive power source in the form of an engine 12, a first electric motor MG1, a second electric motor MG2, a first differential mechanism in the form of a first planetary gear set 14, and a second differential mechanism in the form of a second planetary gear set 16, which are disposed on a common center axis CE. The drive system 10 is constructed substantially symmetrically with respect to the center axis CE. In FIG. 1, a lower half of the drive system 10 is not shown. This description applies to other embodiments which will be described.

The engine 12 is an internal combustion engine such as a gasoline engine, which is operable to generate a drive force by combustion of a fuel such as a gasoline injected into its cylinders. Each of the first electric motor MG1 and second electric motor MG2 is a so-called motor/generator having a function of a motor operable to generate a drive force, and a function of an electric generator operable to generate a reaction force, and is provided with a stator 18, 22 fixed to a stationary member in the form of a housing (casing) 26, and a rotor 20, 24 disposed radially inwardly of the stator 18, 22.

The first planetary gear set 14 is a single-pinion type planetary gear set which has a gear ratio  $\rho 1$  and which is provided with rotary elements (elements) consisting of: a first rotary element in the form of a sun gear S1; a second rotary element in the form of a carrier C1 supporting a pinion gear P1 such that the pinion gear P1 is rotatable about its axis and the axis of the planetary gear set; and a third rotary element in the form of a ring gear R1 meshing with the sun gear S1 through the pinion gear P1. The second planetary gear set 16 is a single-pinion type planetary gear set which has a gear ratio  $\rho 2$  and which is provided with rotary elements (elements) consisting of: a first rotary element in the form of a sun gear S2; a second rotary element in the form of a carrier C2 supporting a pinion gear P2 such that the pinion gear P2 is rotatable about its axis and the axis of the planetary gear set; and a third rotary element in the form of a ring gear R2 meshing with the sun gear S2 through the pinion gear P2.

The sun gear S1 of the first planetary gear set 14 is connected to the rotor 20 of the first electric motor MG1. The carrier C1 of the first planetary gear set 14 is connected to an input shaft 28 which is rotated integrally with a crankshaft of the engine 12. This input shaft 28 is rotated about the center axis CE. In the following description, the direction of extension of this center axis CE will be referred to as an "axial direction", unless otherwise specified. The ring gear R1 of the first planetary gear set 14 is connected to an output rotary member in the form of an output gear 30, and to the ring gear R2 of the second planetary gear set 16. The sun gear S2 of the second planetary gear set 16 is connected to the rotor 24 of the second electric motor MG2.

The drive force received by the output gear 30 is transmitted to a pair of left and right drive wheels (not shown) through a differential gear device not shown and axles not shown. On the other hand, a torque received by the drive wheels from a roadway surface on which the vehicle is running is transmitted (input) to the output gear 30 through the differential gear device and axles, and to the drive system 10. A mechanical oil pump 32, which is a vane pump, for instance, is connected to one of opposite end portions of the input shaft 28, which one end portion is remote from the engine 12. The oil pump 32 is operated by the engine 12, to generate a hydraulic pressure to be applied to a hydraulic control unit 60, etc. which will be described. An electrically operated oil pump which is operated with an electric energy may be provided in addition to the oil pump 32.

Between the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16, there is disposed a clutch CL which is configured to selectively couple these carriers C1 and C2 to each other (to selectively connect the carriers C1 and C2 to each other or disconnect the carriers C1 and C2 from each other). Between the carrier C2 of the second planetary gear set 16 and the stationary member in the form of the housing 26, there is disposed a brake BK which is configured to selectively couple (fix) the carrier C2 to the housing 26. Each of these clutch CL and brake BK is a hydraulically operated coupling device the operating state of which is controlled (which is engaged and released) according to the hydraulic pressure applied thereto from the hydraulic control unit 60. While wet multiple-disc type frictional coupling devices are preferably used as the clutch CL and brake BK, meshing type coupling devices, namely, so-called dog clutches (claw clutches) may also be used. Alternatively, the clutch CL and brake BK may be electromagnetic clutches, magnetic powder clutches and any other clutches the operating states of which are controlled (which are engaged and released) according to electric commands generated from an electronic control device 40.

As shown in FIG. 1, the drive system 10 is configured such that the first planetary gear set 14 and second planetary gear set 16 are disposed coaxially with the input shaft 28 (disposed on the center axis CE), and opposed to each other in the axial direction of the center axis CE. Namely, the first planetary gear set 14 is disposed on one side of the second planetary gear set 16 on a side of the engine 12, in the axial direction of the center axis CE. The first electric motor MG1 is disposed on one side of the first planetary gear set 14 on the side of the engine 12, in the axial direction of the center axis CE. The second electric motor MG2 is disposed on one side of the second planetary gear set 16 which is remote from the engine 12, in the axial direction of the center axis CE. Namely, the first electric motor MG1 and second electric motor MG2 are opposed to each other in the axial direction of the center axis CE, such that the first planetary gear set 14 and second planetary gear set 16 are interposed between the first electric motor MG1 and second electric motor MG2. That is, the drive system 10 is configured such that the first electric motor MG1, first planetary gear set 14, clutch CL, second planetary gear set 16, brake BK and second electric motor MG2 are disposed coaxially with each other, in the order of description from the side of the engine 12, in the axial direction of the center axis CE.

FIG. 2 is the view for explaining major portions of a control system provided to control the drive system 10. The electronic control device 40 shown in FIG. 2 is a so-called micro-computer which incorporates a CPU, a ROM, a RAM and an input-output interface and which is operable to perform signal processing operations according to programs stored in the ROM while utilizing a temporary data storage function of the RAM, to implement various drive controls of the drive system 10, such as a drive control of the engine 12 and hybrid drive controls of the first electric motor MG1 and second electric motor MG2. In the present embodiment, the electronic control device 40 corresponds to a drive control device for a hybrid vehicle having the drive system 10. The electronic control device 40 may be constituted by mutually independent control units as needed for respective controls such as an output control of the engine 12 and drive controls of the first electric motor MG1 and second electric motor MG2.

As indicated in FIG. 2, the electronic control device 40 is configured to receive various signals from sensors and switches provided in the drive system 10. Namely, the electronic control device 40 receives: an output signal of an accel-

erator pedal operation amount sensor 42 indicative of an operation amount or angle  $A_{CC}$  of an accelerator pedal (not shown), which corresponds to a vehicle output required by a vehicle operator; an output signal of an engine speed sensor 44 indicative of an engine speed  $N_E$ , that is, an operating speed of the engine 12; an output signal of an MG1 speed sensor 46 indicative of an operating speed  $N_{MG1}$  of the first electric motor MG1; an output signal of an MG2 speed sensor 48 indicative of an operating speed  $N_{MG2}$  of the second electric motor MG2; an output signal of an output speed sensor 50 indicative of a rotating speed  $N_{OUT}$  of the output gear 30, which corresponds to a running speed V of the vehicle; an output signal of an MG1 temperature sensor 52 indicative of a temperature  $T_{m_{MG1}}$  of the first electric motor MG1; and an output signal of an MG2 temperature sensor 53 indicative of a temperature  $T_{m_{MG2}}$  of the second electric motor MG2; and an output signal of a battery SOC sensor 54 indicative of a stored electric energy amount (state of charge) SOC of a battery not shown.

The electronic control device 40 is also configured to generate various control commands to be applied to various portions of the drive system 10. Namely, the electronic control device 40 applies to an engine control device 56 for controlling an output of the engine 12, following engine output control commands for controlling the output of the engine 12, which commands include: a fuel injection amount control signal to control an amount of injection of a fuel by a fuel injecting device into an intake pipe; an ignition control signal to control a timing of ignition of the engine 12 by an igniting device; and an electronic throttle valve drive control signal to control a throttle actuator for controlling an opening angle  $\theta_{TH}$  of an electronic throttle valve. Further, the electronic control device 40 applies command signals to an inverter 58, for controlling operations of the first electric motor MG1 and second electric motor MG2, so that the first and second electric motors MG1 and MG2 are operated with electric energies supplied thereto from a battery through the inverter 58 according to the command signals to control outputs (output torques) of the electric motors MG1 and MG2. Electric energies generated by the first and second electric motors MG1 and MG2 are supplied to and stored in the battery through the inverter 58. Further, the electronic control device 40 applies command signals for controlling the operating states of the clutch CL and brake BK, to linear solenoid valves and other electromagnetic control valves provided in the hydraulic control unit 60, so that hydraulic pressures generated by those electromagnetic control valves are controlled to control the operating states of the clutch CL and brake BK.

An operating state of the drive system 10 is controlled through the first electric motor MG1 and second electric motor MG2, such that the drive system 10 functions as an electrically controlled differential portion whose difference of input and output speeds is controllable. For example, an electric energy generated by the first electric motor MG1 is supplied to the battery or the second electric motor MG2 through the inverter 58. Namely, a major portion of the drive force of the engine 12 is mechanically transmitted to the output gear 30, while the remaining portion of the drive force is consumed by the first electric motor MG1 operating as the electric generator, and converted into the electric energy, which is supplied to the second electric motor MG2 through the inverter 58, so that the second electric motor MG2 is operated to generate a drive force to be transmitted to the output gear 30. Components associated with the generation of the electric energy and the consumption of the generated electric energy by the second electric motor MG2 constitute an electric path through which a portion of the drive force of

the engine 12 is converted into an electric energy which is converted into a mechanical energy.

In the hybrid vehicle provided with the drive system 10 constructed as described above, one of a plurality of drive modes is selectively established according to the operating states of the engine 12, first electric motor MG1 and second electric motor MG2, and the operating states of the clutch CL and brake BK. FIG. 3 is the table indicating combinations of the operating states of the clutch CL and brake BK, which correspond to the respective five drive modes of the drive system 10. In this table, "o" marks represent an engaged state while blanks represent a released state. The drive modes EV-1 and EV-2 indicated in FIG. 3 are EV drive modes in which the engine 12 is held at rest while at least one of the first electric motor MG1 and second electric motor MG2 is used as a vehicle drive power source. The drive modes HV-1, HV-2 and HV-3 are hybrid drive modes (HV modes) in which the engine 12 is operated as the vehicle drive power source while the first electric motor MG1 and second electric motor MG2 are operated as needed to generate a vehicle drive force and/or an electric energy. In these hybrid drive modes, at least one of the first electric motor MG1 and second electric motor MG2 is operated to generate a reaction force or placed in a non-load free state.

As is apparent from FIG. 3, the EV drive modes of the drive system 10 in which the engine 12 is held at rest while at least one of the first electric motor MG1 and second electric motor MG2 is used as the vehicle drive power source consist of: a mode 1 (drive mode 1) in the form of the drive mode EV-1 which is established in the engaged state of the brake BK and in the released state of the clutch CL; and a mode 2 (drive mode 2) in the form of the drive mode EV-2 which is established in the engaged states of both of the brake BK and clutch CL. The hybrid drive modes in which the engine 12 is operated as the vehicle drive power source while the first electric motor MG1 and second electric motor MG2 are operated as needed to generate a vehicle drive force and/or an electric energy, consist of: a mode 3 (drive mode 3) in the form of the drive mode HV-1 which is established in the engaged state of the brake BK and in the released state of the clutch CL; a mode 4 (drive mode 4) in the form of the drive mode HV-2 which is established in the released state of the brake BK and in the engaged state of the clutch CL; and a mode 5 (drive mode 5) in the form of the drive mode HV-3 which is established in the released states of both of the brake BK and clutch CL.

FIGS. 4-7 are the collinear charts having straight lines which permit indication thereon of relative rotating speeds of the various rotary elements of the drive system 10 (first planetary gear set 14 and second planetary gear set 16), which rotary elements are connected to each other in different manners corresponding to respective combinations of the operating states of the clutch CL and brake BK. These collinear charts are defined in a two-dimensional coordinate system having a horizontal axis along which relative gear ratios  $\rho$  of the first and second planetary gear sets 14 and 16 are taken, and a vertical axis along which the relative rotating speeds are taken. The collinear charts indicate the relative rotating speeds when the output gear 30 is rotated in the positive direction to drive the hybrid vehicle in the forward direction. A horizontal line X1 represents the rotating speed of zero, while vertical lines Y1 through Y4 arranged in the order of description in the rightward direction represent the respective relative rotating speeds of the sun gear S1, sun gear S2, carrier C1 and ring gear R1. Namely, a solid line Y1 represents the relative rotating speed of the sun gear S1 of the first planetary gear set 14 (operating speed of the first electric motor MG1),

a broken line Y2 represents the relative rotating speed of the sun gear S2 of the second planetary gear set 16 (operating speed of the second electric motor MG2), a solid line Y3 represents the relative rotating speed of the carrier C1 of the first planetary gear set 14 (operating speed of the engine 12), a broken line Y3' represents the relative rotating speed of the carrier C2 of the second planetary gear set 16, a solid line Y4 represents the relative rotating speed of the ring gear R1 of the first planetary gear set 14 (rotating speed of the output gear 30), and a broken line Y4' represents the relative rotating speed of the ring gear R2 of the second planetary gear set 16. In FIGS. 4-7, the vertical lines Y3 and Y3' are superimposed on each other, while the vertical lines Y4 and Y4' are superimposed on each other. Since the ring gears R1 and R2 are fixed to each other, the relative rotating speeds of the ring gears R1 and R2 represented by the vertical lines Y4 and Y4' are equal to each other.

In FIGS. 4-7, a solid line L1 represents the relative rotating speeds of the three rotary elements of the first planetary gear set 14, while a broken line L2 represents the relative rotating speeds of the three rotary elements of the second planetary gear set 16. Distances between the vertical lines Y1-Y4 (Y2-Y4') are determined by the gear ratios  $\rho_1$  and  $\rho_2$  of the first and second planetary gear sets 14 and 16. Described more specifically, regarding the vertical lines Y1, Y3 and Y4 corresponding to the respective three rotary elements in the form of the sun gear S1, carrier C1 and ring gear R1 of the first planetary gear set 14, a distance between the vertical lines Y1 and Y3 corresponds to "1", while a distance between the vertical lines Y3 and Y4 corresponds to the gear ratio " $\rho_1$ ". Regarding the vertical lines Y2, Y3' and Y4' corresponding to the respective three rotary elements in the form of the sun gear S2, carrier C2 and ring gear R2 of the second planetary gear set 16, a distance between the vertical lines Y2 and Y3' corresponds to "1", while a distance between the vertical lines Y3' and Y4' corresponds to the gear ratio " $\rho_2$ ". In the drive system 10, the gear ratio  $\rho_2$  of the second planetary gear set 16 is higher than the gear ratio  $\rho_1$  of the first planetary gear set 14 ( $\rho_2 > \rho_1$ ). The drive modes of the drive system 10 will be described by reference to FIGS. 4-7.

The drive mode EV-1 indicated in FIG. 3 corresponds to the mode 1 (drive mode 1) of the drive system 10, which is preferably the EV drive mode in which the engine 12 is held at rest while the second electric motor MG2 is used as the vehicle drive power source. FIG. 4 is the collinear chart corresponding to the mode 1. Described by reference to this collinear chart, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are rotatable relative to each other in the released state of the clutch CL. In the engaged state of the brake BK, the carrier C2 of the second planetary gear set 16 is coupled (fixed) to the stationary member in the form of the housing 26, so that the rotating speed of the carrier C2 is held zero. In this mode 1, the rotating direction of the sun gear S2 and the rotating direction of the ring gear R2 in the second planetary gear set 16 are opposite to each other, so that when the second electric motor MG2 is operated to generate a negative torque (acting in the negative direction), the ring gear R2, that is, the output gear 30 is rotated in the positive direction by the generated negative torque. Namely, the hybrid vehicle provided with the drive system 10 is driven in the forward direction when the negative torque is generated by the second electric motor MG2. In this case, the first electric motor MG1 is preferably held in a free state. In this mode 1, the carriers C1 and C2 are permitted to be rotated relative to each other, so that the hybrid vehicle can be driven in the EV drive mode similar to an EV drive mode which is established in a vehicle provided with a so-called

## 11

“THS” (Toyota Hybrid System) and in which the carrier C2 is fixed to the stationary member.

The drive mode EV-2 indicated in FIG. 3 corresponds to the mode 2 (drive mode 2) of the drive system 10, which is preferably the EV drive mode in which the engine 12 is held at rest while at least one of the first electric motor MG1 and second electric motor MG2 is used as the vehicle drive power source. FIG. 5 is the collinear chart corresponding to the mode 2. Described by reference to this collinear chart, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are not rotatable relative to each other in the engaged state of the clutch CL. Further, in the engaged state of the brake BK, the carrier C2 of the second planetary gear set 16 and the carrier C1 of the first planetary gear set 14 which is connected to the carrier C2 are coupled (fixed) to the stationary member in the form of the housing 26, so that the rotating speeds of the carriers C1 and C2 are held zero. In this mode 2, the rotating direction of the sun gear S1 and the rotating direction of the ring gear R1 in the first planetary gear set 14 are opposite to each other, and the rotating direction of the sun gear S2 and the rotating direction of the ring gear R2 in the second planetary gear set 16 are opposite to each other, so that when the first electric motor MG1 and/or second electric motor MG2 is/are operated to generate a negative torque (acting in the negative direction), the ring gears R1 and R2 are rotated, that is, the output gear 30 is rotated in the positive direction by the generated negative torque. Namely, the hybrid vehicle provided with the drive system 10 is driven in the forward direction when the negative torque is generated by at least one of the first electric motor MG1 and second electric motor MG2.

In the mode 2, at least one of the first electric motor MG1 and second electric motor MG2 may be operated as the electric generator. In this case, one or both of the first and second electric motors MG1 and MG2 may be operated to generate a vehicle drive force (torque), at an operating point assuring a relatively high degree of operating efficiency, and/or with a reduced degree of torque limitation due to heat generation. Further, at least one of the first and second electric motors MG1 and MG2 may be held in a free state, when the generation of an electric energy by a regenerative operation of the electric motors MG1 and MG2 is inhibited due to full charging of the battery. Namely, the mode 2 is an EV drive mode in which may be established under various running conditions of the hybrid vehicle, or may be kept for a relatively long length of time. Accordingly, the mode 2 is advantageously provided on a hybrid vehicle such as a plug-in hybrid vehicle, which is frequently placed in an EV drive mode.

The drive mode HV-1 indicated in FIG. 3 corresponds to the mode 3 (drive mode 3) of the drive system 10, which is preferably the HV drive mode in which the engine 12 is used as the vehicle drive power source while the first electric motor MG1 and second electric motor MG2 are operated as needed to generate a vehicle drive force and/or an electric energy. FIG. 4 is the collinear chart corresponding to the mode 3. Described by reference to this collinear chart, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are rotatable relative to each other, in the released state of the clutch CL. In the engaged state of the brake BK, the carrier C2 of the second planetary gear set 16 is coupled (fixed) to the stationary member in the form of the housing 26, so that the rotating speed of the carrier C2 is held zero. In this mode 3, the engine 12 is operated to generate an output torque by which the output gear 30 is rotated. At this time, the first electric motor MG1 is operated to generate a reaction torque in the first planetary gear set 14, so that the output of the engine 12 can be transmitted to the

## 12

output gear 30. In the second planetary gear set 16, the rotating direction of the sun gear S2 and the rotating direction of the ring gear R2 are opposite to each other, in the engaged state of the brake BK, so that when the second electric motor MG2 is operated to generate a negative torque (acting in the negative direction), the ring gears R1 and R2 are rotated, that is, the output gear 30 is rotated in the positive direction by the generated negative torque.

The drive mode HV-2 indicated in FIG. 3 corresponds to the mode 4 (drive mode 4) of the drive system 10, which is preferably the HV drive mode in which the engine 12 is used as the vehicle drive power source while the first electric motor MG1 and second electric motor MG2 are operated as needed to generate a vehicle drive force and/or an electric energy. FIG. 6 is the collinear chart corresponding to the mode 4. Described by reference to this collinear chart, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are not rotatable relative to each other, in the engaged state of the clutch CL, that is, the carriers C1 and C2 are integrally rotated as a single rotary element. The ring gears R1 and R2, which are fixed to each other, are integrally rotated as a single rotary element. Namely, in the mode 4 of the drive system 10, the first planetary gear set 14 and second planetary gear set 16 function as a differential mechanism having a total of four rotary elements. That is, the drive mode 4 is a composite split mode in which the four rotary elements consisting of the sun gear S1 (connected to the first electric motor MG1), the sun gear S2 (connected to the second electric motor MG2), the rotary element constituted by the carriers C1 and C2 connected to each other (and to the engine 12), and the rotary element constituted by the ring gears R1 and R2 fixed to each other (and connected to the output gear 30) are connected to each other in the order of description in the rightward direction as seen in FIG. 6.

In the mode 4, the rotary elements of the first planetary gear set 14 and second planetary gear set 16 are preferably arranged as indicated in the collinear chart of FIG. 6, that is, in the order of the sun gear S1 represented by the vertical line Y1, the sun gear S2 represented by the vertical line Y2, the carriers C1 and C2 represented by the vertical line Y3 (Y3'), and the ring gears R1 and R2 represented by the vertical line Y4 (Y4'). The gear ratios  $\rho_1$  and  $\rho_2$  of the first and second planetary gear sets 14 and 16 are determined such that the vertical line Y1 corresponding to the sun gear S1 and the vertical line Y2 corresponding to the sun gear S2 are positioned as indicated in the collinear chart of FIG. 6, namely, such that the distance between the vertical lines Y1 and Y3 is longer than the distance between the vertical lines Y2 and Y3'. In other words, the distance between the vertical lines corresponding to the sun gear S1 and the carrier C1 and the distance between the vertical lines corresponding to the sun gear S2 and the carrier C2 correspond to “1”, while the distance between the vertical lines corresponding to the carrier C1 and the ring gear R1 and the distance between the vertical lines corresponding to the carrier C2 and the ring gear R2 correspond to the respective gear ratios  $\rho_1$  and  $\rho_2$ . Accordingly, the drive system 10 is configured such that the gear ratio  $\rho_2$  of the second planetary gear set 16 is higher than the gear ratio  $\rho_1$  of the first planetary gear set 14.

In the mode 4, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are connected to each other in the engaged state of the clutch CL, so that the carriers C1 and C2 are rotated integrally with each other. Accordingly, either one or both of the first electric motor MG1 and second electric motor MG2 can receive a reaction force corresponding to the output of the engine 12. Namely, one or both of the first and second electric motors

## 13

MG1 and MG2 can be operated to receive the reaction force during an operation of the engine 12, at an operating point assuring a relatively high degree of operating efficiency, and/or with a reduced degree of torque limitation due to heat generation. For example, one of the first electric motor MG1 and second electric motor MG2 which is operable with a higher degree of operating efficiency is preferentially operated to generate a reaction force, so that the overall operating efficiency can be improved. Further, where there is a torque limitation of one of the first electric motor MG1 and second electric motor MG2 due to heat generation, it is possible to ensure the generation of the reaction force required for the engine 12, by controlling the other electric motor so as to perform a regenerative operation or a vehicle driving operation, for providing an assisting vehicle driving force.

The drive mode HV-3 indicated in FIG. 3 corresponds to the mode 5 (drive mode 5) of the drive system 10, which is preferably the hybrid drive mode in which the engine 12 is operated as the vehicle drive power source while the first electric motor MG1 is operated as needed to generate a vehicle drive force and/or an electric energy. In this mode 5, the engine 12 and first electric motor MG1 may be operated to generate a vehicle drive force, with the second electric motor MG2 being disconnected from a drive system. FIG. 7 is the collinear chart corresponding to this mode 5. Described by reference to this collinear chart, the carrier C1 of the first planetary gear set 14 and the carrier C2 of the second planetary gear set 16 are rotatable relative to each other in the released state of the clutch CL. In the released state of the brake BK, the carrier C2 of the second planetary gear set 16 is rotatable relative to the stationary member in the form of the housing 26. In this arrangement, the second electric motor MG2 can be held at rest while it is disconnected from the drive system (power transmitting path).

In the mode 3 in which the brake BK is placed in the engaged state, the second electric motor MG2 is kept in an operated state together with a rotary motion of the output gear 30 (ring gear R2) during running of the vehicle. In this operating state, the operating speed of the second electric motor MG2 may reach an upper limit value (upper limit) during running of the vehicle at a comparatively high speed, or a rotary motion of the ring gear R2 at a high speed is transmitted to the sun gear S2. In this respect, it is not necessarily desirable to keep the second electric motor MG2 in the operated state during running of the vehicle at a comparatively high speed, from the standpoint of the operating efficiency. In the mode 5, on the other hand, the engine 12 and the first electric motor MG1 may be operated to generate the vehicle drive force during running of the vehicle at the comparatively high speed, while the second electric motor MG2 is disconnected from the drive system, so that it is possible to reduce a power loss due to dragging of the unnecessarily operated second electric motor MG2, and to eliminate a limitation of the highest vehicle running speed corresponding to the permissible highest operating speed (upper limit of the operating speed) of the second electric motor MG2.

It will be understood from the foregoing description, the drive system 10 is selectively placed in one of the three hybrid drive modes in which the engine 12 is operated as the vehicle drive power source, namely, in one of the drive mode HV-1 (mode 3), drive mode HV-2 (mode 4) and drive mode HV-3 (mode 5), which are selectively established by respective combinations of the engaged and released states of the clutch CL and brake BK. Accordingly, the transmission efficiency can be improved to improve the fuel economy of the vehicle, by selectively establishing one of the three hybrid drive

## 14

modes according to the vehicle running speed and the speed ratio, in which the transmission efficiency is the highest.

FIG. 8 is the functional block diagram for explaining major control functions of the electronic control device 40. An engine starting requirement determining portion 70 shown in FIG. 8 is configured to determine whether the engine 12 which has been held at rest is required to be started. For instance, the engine starting requirement determining portion 70 determines a requirement for starting the engine 12, if the stored electric energy amount SOC detected by the battery SOC sensor 54 upon starting of the vehicle is equal to or smaller than a predetermined value. Further, the engine starting requirement determining portion 70 may determine the requirement for starting the engine 12, in a running state of the vehicle, depending upon the drive mode which is required to be established on the basis of the accelerator pedal operation amount  $A_{CC}$  detected by the accelerator pedal operation amount sensor 42, the output speed  $N_{OUT}$  detected by the output speed sensor 50 and corresponding to the vehicle running speed  $V$ , and the stored electric energy amount SOC detected by the battery SOC sensor 54. Namely, the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, if the vehicle drive mode is required to be switched from one of the EV drive modes in which at least one of the first and second electric motors MG1 and MG2 is operated as the vehicle drive power source while the engine 12 is held at rest, to one of the hybrid drive modes in which the engine 12 is operated. Described more specifically, the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, when the vehicle drive mode is determined to switch from one of the mode 1 (EV-1) and the mode 2 (EV-2) indicated in FIG. 3, to one of the mode 3 (HV-1), the mode 4 (HV-2) and the mode 5 (HV-3) also indicated in FIG. 3. For instance, the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, on the basis of the determination that the vehicle drive mode should be switched from one of the above-indicated EV drive modes to one of the hybrid drive modes, as a result of the determination that the stored electric energy amount SOC detected by the battery SOC sensor 54 has been reduced to or below the predetermined value.

A clutch engagement control portion 72 is configured to control the operating state of the clutch CL through the hydraulic control unit 60. For instance, the clutch engagement control portion 72 controls an output hydraulic pressure of an electromagnetic control valve provided in the hydraulic control unit 60 to control the clutch CL, so as to place the clutch CL in an engaged state or a released state. A brake engagement control portion 74 is configured to control the operating state of the brake BK through the hydraulic control unit 60. For instance, the brake engagement control portion 74 controls an output hydraulic pressure of an electromagnetic control valve provided in the hydraulic control unit 60 to control the brake BK, so as to place the brake BK in an engaged state or a released state. The clutch engagement control portion 72 and the brake engagement control portion 74 are basically configured to control the operating states of the clutch CL and the brake BK to establish the vehicle drive mode selected according to the running state of the hybrid vehicle. Namely, the clutch and brake engagement control portions 72 and 74 establish one of the combinations of the operating states of the clutch CL and the brake BK indicated in FIG. 3, which corresponds to one of the modes 1-5 to be established.

An electric motor operation control portion 76 is configured to control the operations of the first and second electric motors MG1 and MG2 through the inverter 58. Described

more specifically, the electric motor operation control portion **76** controls amounts of electric energy to be supplied from the battery not shown, to the first and second electric motors **MG1** and **MG2** through the inverter **58**, so that each of the first and second electric motors **MG1** and **MG2** provides a required output, that is, a target torque (target electric motor output). When the first or second electric motor **MG1**, **MG2** is operated as an electric generator, the electric motor operation control portion **76** implements a control for storing an electric energy generated by the first or second electric motor **MG1**, **MG2**, in the battery through the inverter **58**.

An **MG1** failure determining portion **78** is configured to determine a failure of the first electric motor **MG1**. Namely, the **MG1** failure determining portion **78** determines whether the first electric motor **MG1** has an operational defect preventing its normal operation. For example, the **MG1** failure determining portion **78** makes the determination as to whether the first electric motor **MG1** has an operational defect, on the basis of a difference of the first electric motor speed  $N_{MG1}$  detected by the **MG1** speed sensor **46**, with respect to a value of a command generated from the electric motor operation control portion **76** to specify the output of the first electric motor **MG1**. Described more specifically, the **MG1** failure determining portion **78** determines a failure of the first electric motor **MG1**, if the difference of the first electric motor speed  $N_{MG1}$  detected by the **MG1** speed sensor **46** with respect to the value of the command generated from the electric motor operation control portion **76** to specify the output of the first electric motor **MG1** has become equal to or larger than a predetermined value.

A torque limitation determining portion **80** is configured to determine whether the torque of at least one of the first and second electric motors **MG1** and **MG2** should be limited. That is, the torque limitation determining portion **80** determines whether the torque of at least one of the first and second electric motors **MG1** and **MG2** should be limited to or below a predetermined upper limit. For instance, the torque limitation determining portion **80** determines that the torque of the first electric motor **MG1** should be limited to or below the predetermined upper limit, if the first electric motor **MG1** is overheated with a rise of its temperature  $T_{m, MG1}$  detected by the **MG1** temperature sensor **52** to a value equal to or higher than a predetermined threshold value, and determines that the torque of the second electric motor **MG2** should be limited to or below the predetermined upper limit, if the second electric motor **MG2** is overheated with a rise of its temperature  $T_{m, MG2}$  detected by the **MG2** temperature sensor **53** to a value equal to or higher than a predetermined threshold value. Further, the torque limitation determining portion **80** determines that the torques of the first and second electric motors **MG1** and **MG2** should be limited to or below the respective upper limits, if the stored electric energy amount **SOC** detected by the battery **SOC** sensor **54** is smaller than a predetermined threshold value. Preferably, the above-indicated upper limits are suitably determined to be different values, depending upon the different situations.

An **MG2** speed determining portion **82** is configured to determine whether a rotary motion speed  $N_{MG2}$  of the second electric motor **MG2** has become equal to or higher than a predetermined threshold value  $N_{bo}$ . This threshold value  $N_{bo}$  corresponds to an inertia force required to crank the engine **12** for starting the engine **12**. Preferably, the threshold value  $N_{bo}$  is a value (constant value) predetermined by experimentation. That is, the threshold value  $N_{bo}$  is a value at which a torque required to crank the engine **12** is obtained by an inertia force (rotary motion inertia) of the rotor **24** when the clutch **CL** is

brought into the engaged state after the rotary motion speed  $N_{MG2}$  of the second electric motor **MG2** is raised to that threshold value  $N_{bo}$ .

When the engine starting requirement determining portion **70** determines the requirement for starting the engine **12**, the electric motor operation control portion **76** controls the operation of at least one of the first and second electric motors **MG1** and **MG2**, to crank the engine **12**. Namely, the electric motor operation control portion **76** controls the torque of at least one of the first and second electric motors **MG1** and **MG2**, to raise the rotating speed of the input shaft **28** (rotating speed of the carrier **C1**) corresponding to the rotating speed of the crankshaft of the engine **12**. After the rotating speed of the crankshaft of the engine **12** has been raised to a predetermined value, the engine control device **56** initiates a control to permit an operation of the engine **12** by itself. An engine starting control described below may be implemented for starting the engine **12** upon starting of the hybrid vehicle (upon vehicle starting) while the hybrid vehicle is stationary, or during running of the hybrid vehicle.

When the engine starting requirement determining portion **70** determines the requirement for starting the engine **12**, it is preferable that the clutch engagement control portion **72** brings the clutch **CL** into the engaged state, and while the electric motor operation control portion **76** controls the operation of the second electric motor **MG2** to crank the engine **12** with the output torque of the second electric motor **MG2**. In the drive system **10**, the engine **12** and the second electric motor **MG2** are directly connected to each other in the engaged state of the clutch **CL**, and a reaction force is exerted on the first and second electric motors **MG1** and **MG2**. In other words, when the engine starting requirement determining portion **70** determines the requirement for starting the engine **12** while a reaction force is exerted on the first and second electric motors **MG1** and **MG2**, the electric motor operation control portion **76** controls the operation of the second electric motor **MG2**, to crank the engine **12** with the output torque of the second electric motor **MG2**. Preferably, the clutch **CL** is brought into the engaged state while the brake **BK** is brought into the released state, and the engine **12** is cranked primarily by the output torque of the second electric motor **MG2**. In this case, the drive mode **HV-2** (mode **4**) indicated in **FIG. 3** is established after the engine **12** has been started. Where the engine **12** is started by the second electric motor **MG2** as described above, the torque of the first electric motor **MG1** is preferably controlled so as to prevent the drive shaft from receiving a reaction force. In the drive system **10**, the gear ratio  $\rho_2$  of the second planetary gear set **16** is higher than the gear ratio  $\rho_1$  of the first planetary gear set **14**, as described above. Accordingly, where the engine **12** is cranked by the output torque of the second electric motor **MG2**, the engine cranking torque is larger than where the engine **12** is cranked by the output torque of the first electric motor **MG1**, so that a rotary motion speed of the engine **12** can be rapidly raised through a resonance band of a power transmitting system, whereby a starting shock of the engine **12** can be reduced.

When the engine starting requirement determining portion **70** determines the requirement for starting the engine **12**, it is preferable that the clutch engagement control portion **72** brings the clutch **CL** into the engaged state while the brake engagement control portion **74** brings the brake **BK** into the released state, and the electric motor operation control portion **76** controls the operations of the first and second electric motors **MG1** and **MG2**, to crank the engine **12** with the output torques of the first and second electric motors **MG1** and **MG2**. Where the engine **12** is cranked with a sum of the output

17

torques of the first and second electric motors MG1 and MG2, the engine cranking torque is larger than where the engine 12 is cranked by the output torque of only one of the first and second electric motors MG1 and MG2, so that the rotary motion speed of the engine 12 can be more rapidly raised through the resonance band of the power transmitting system, whereby the starting shock of the engine 12 can be reduced.

When the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, while the output torque of the first electric motor MG1 should be limited due to a failure or overheating of the first electric motor MG1, for example, it is preferable that the clutch CL is brought into the engaged state while the brake BK is brought into the released state, and the engine 12 is started primarily with the output torque of the second electric motor MG2. Where the MG1 failure determining portion 78 determines a failure of the first electric motor MG1, the clutch CL is brought into the engaged state while the brake BK is brought into the released state, and the engine 12 is started primarily with the output torque of the second electric motor MG2. Where the upper limit of the output torque of the first electric motor MG1 used by the torque limitation determining portion 80 is smaller than the torque required to crank the engine 12, the clutch CL is brought into the engaged state while the brake BK is brought into the released state, and the engine 12 is started primarily with the output torque of the second electric motor MG2.

When the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, while the output torque of the first electric motor MG1 should be limited due to a failure or overheating of the first electric motor MG1, and while the torque required to crank the engine 12 cannot be generated by the second electric motor MG2, the clutch CL and the brake BK are both brought into the released state, and the clutch CL is brought into the engaged state to start the engine 12 after the speed  $N_{MG2}$  of the second electric motor MG2 is raised in a freely rotatable state. Preferably, this manner of engine starting control is implemented where the MG1 failure determining portion 78 determines a failure of the first electric motor MG1 while the upper limit of the output torque of the second electric motor MG2 used by the torque limitation determining portion 80 is smaller than the torque required to crank the engine 12. This manner of engine starting control is preferably implemented where the upper limits of the output torques of the first and second electric motors MG1 and MG2 used by the torque limitation determining portion 80 are both smaller than the torque required to crank the engine 12. Described more specifically, the clutch engagement control portion 72 and the brake engagement control portion 74 bring the respective clutch CL and brake BK into the released state, the electric motor operation control portion 78 places the second electric motor MG2 in the freely rotatable state to permit a rise of its speed  $N_{MG2}$ , and the clutch engagement control portion 72 brings the clutch CL into the engaged state after the MG2 speed determining portion 82 determines that the speed  $N_{MG2}$  of the second electric motor MG2 has been raised to or above the predetermined threshold value  $N_{bo}$ . This manner of engine starting control permits cranking of the engine 12 with a sufficient torque, so that the operation of the engine 12 by itself is initiated under the control of the engine control device 56 after the rotating speed of the crankshaft of the engine 12 has been raised to the predetermined value.

When the engine starting requirement determining portion 70 determines the requirement for starting the engine 12, in the event of a failure of the brake BK, that is, while the brake BK fails to normally function due to a hydraulic defect in the

18

hydraulic control unit 60, for example, the clutch engagement control portion 72 brings the clutch CL into the engaged state, and the electric motor operation control portion 76 controls the operation of the second electric motor MG2 to crank the engine 12 with the output torque of the second electric motor MG2. If the engine 12 was started with the output torque of the first electric motor MG1 while the brake BK has a failure, the reaction force generated during starting of the engine 12 could not be offset, so that a vehicle drive force would be transmitted to an output side (drive shaft), giving rise to a risk of an adverse influence on a behavior of the hybrid vehicle, causing the vehicle operator to feel uneasy about the vehicle behavior. Where the engine 12 is started with the output torque of the second electric motor MG2 as described above in the event of a failure of the brake BK, on the other hand, it is possible to prevent transmission of a drive force to the output side, for suitably preventing an adverse influence on the vehicle behavior.

FIG. 9 is the flow chart for explaining a major portion of an example of an engine starting control implemented by the electronic control device 40. The engine starting control is repeatedly implemented with a predetermined cycle time.

The engine starting control is initiated with step SA1 ("step" being hereinafter omitted), to determine whether the first electric motor MG1 fails to normally function while the engine 12 is required to be started. If a negative determination is obtained in SA1, the control flow goes to SA2 to crank the engine 12 with the output torque of the first electric motor MG1, to start the engine 12, and the present routine is terminated. If an affirmative determination is obtained in SA1, the control flow goes to SA3 to determine whether the second electric motor MG2 can generate a torque required to crank the engine 12 for starting the engine 12. If an affirmative determination is obtained in SA3, the control flow goes to SA4 to bring the clutch CL into the engaged state and to bring the brake BK into the released state, and to SA5 to crank the engine 12 primarily with the output torque of the second electric motor MG2 for starting the engine 12. Then, the present routine is terminated. If a negative determination is obtained in SA3, the control flow goes to SA6 to bring both of the clutch CL and the brake BK into the released state, and places the second electric motor MG2 in the freely rotatable state to permit a rise of its speed  $N_{MG2}$ . The control flow then goes to SA7 to determine whether the speed  $N_{MG2}$  of the second electric motor MG2 is higher than the predetermined threshold value  $N_{bo}$ . As long as a negative determination is obtained in SA7, this step is repeatedly implemented. If an affirmative determination is obtained in SA7, the control flow goes to SA8 to bring the clutch CL into the engaged state, for cranking the engine 12 to start the engine 12, and the present routine is terminated.

FIG. 10 is the flow chart for explaining a major portion of another example of the engine starting control implemented by the electronic control device 40. This engine starting control is repeatedly implemented with a predetermined cycle time.

This engine starting control is initiated with SB1 to determine whether the output torque of the first electric motor MG1 should be limited due to a rise of the temperature of the first electric motor MG1 to or above the predetermined upper limit while the engine 12 is required to be started. If a negative determination is obtained in SB1, the control flow goes to SB2 to crank the engine 12 with the output torque of the first electric motor MG1, for starting the engine 12, and the present routine is terminated. If an affirmative determination is obtained in SB 1, the control flow goes to SB3 to bring the clutch CL into the engaged state and to bring the brake BK

into the released state. Then, the control flow goes to SB4 to crank the engine 12 with the output torques of the first electric motor and the second electric motor MG2 (or primarily with the output torque of the second electric motor MG2), for starting the engine 12, and the present routine is terminated.

FIG. 11 is the flow chart for explaining a major portion of a further example of the engine starting control implemented by the electronic control device 40. This engine starting control is repeatedly implemented with a predetermined cycle time.

This engine starting control is initiated with SC1, to determine whether the output torques of the first and second electric motors MG1 and MG2 should be limited due to excessive reduction of the stored electric energy amount SOC or rises of the temperatures of the first and second electric motors MG1 and MG2 to or above the predetermined upper limits while the engine 12 is required to be started. If a negative determination is obtained in SC1, the control flow goes to SC2 to crank the engine 12 with the output torque of the first electric motor MG1, for starting the engine 12, and the present routine is terminated. If an affirmative determination is obtained in SC1, the control flow goes to SC3 to bring both of the clutch CL and the brake BK into the released state. Then, the control flow goes to SC4 to place the second electric motor MG2 in the freely rotatable state to permit a rise of its speed  $N_{MG2}$ . Then, the control flow goes to SC5 to determine whether the speed  $N_{MG2}$  of the second electric motor MG2 is equal to or higher than the predetermined threshold value  $N_{bo}$ . As long as a negative determination is obtained in SC5, this step is repeatedly implemented. If an affirmative determination is obtained in SC5, the control flow goes to SC6 to bring the clutch CL into the engaged state, to crank the engine 12 for starting the engine 12, and the present routine is terminated.

It will be understood from the foregoing description that SA1, SB1 and SC1 correspond to the operation of the engine starting requirement determining portion 70, and SA4, SA8, SB3, SC3 and SC6 correspond to the operation of the clutch engagement control portion 72, while SA4, SB3 and SC3 correspond to the operation of the brake engagement control portion 74, and that SA2, SA5, SA6, SB2, SB4, SC2 and SC4 correspond to the operation of the electric motor operation control portion 76, SA1 corresponds to the operation of the MG1 failure determining portion 78, SB1 and SC1 correspond to the operation of the torque limitation determining portion 80, while SA7 and SC5 correspond to the operation of the MG2 speed determining portion 82.

Other preferred embodiments of the present invention will be described in detail by reference to the drawings. In the following description, the same reference signs will be used to identify the same elements in the different embodiments, which will not be described redundantly.

#### Second Embodiment

FIGS. 12-17 are the schematic views for explaining arrangements of respective hybrid vehicle drive systems 100, 110, 120, 130, 140 and 150 according to other preferred modes of this invention. The hybrid vehicle drive control device of the present invention is also applicable to drive systems such as the drive system 100 shown in FIG. 12 and the drive system 110 shown in FIG. 13, which have respective different arrangements of the first electric motor MG1, first planetary gear set 14, second electric motor MG2 and second planetary gear set 16, clutch CL and brake BK in the direction of the center axis CE. The present hybrid vehicle drive control device is also applicable to drive systems such as the drive system 120 shown in FIG. 14, which have a one-way clutch OWC disposed between the carrier C2 of the second planetary gear set 16 and the stationary member in the form of the

housing 26, such that the one-way clutch OWC permits a rotary motion of the carrier C2 relative to the housing 26 in one of opposite directions and inhibits a rotary motion of the carrier C2 in the other direction. The present hybrid vehicle drive control device is further applicable to drive systems such as the drive system 130 shown in FIG. 15, the drive system 140 shown in FIG. 16 and the drive system 150 shown in FIG. 17, each of which is provided with a second differential mechanism in the form of a second planetary gear set 16' of a double-pinion type, in place of the second planetary gear set 16 of a single-pinion type. This second planetary gear set 16' is provided with rotary elements (elements) consisting of: a first rotary element in the form of a sun gear S2'; a second rotary element in the form of a carrier C2' supporting a plurality of pinion gears P2' meshing with each other such that each pinion gear P2' is rotatable about its axis and the axis of the planetary gear set; and a third rotary element in the form of a ring gear R2' meshing with the sun gear S2' through the pinion gears P2'.

#### Third Embodiment

FIGS. 18-20 are the collinear charts for explaining arrangements and operations of respective hybrid vehicle drive systems 160, 170 and 180 according to other preferred embodiments of this invention in place of the drive system 10. In FIGS. 18-20, the relative rotating speeds of the sun gear S1, carrier C1 and ring gear R1 of the first planetary gear set 14 are represented by the solid line L1, while the relative rotating speeds of the sun gear S2, carrier C2 and ring gear R2 of the second planetary gear set 16 are represented by the broken line L2, as in FIGS. 4-7. In the drive system 160 for the hybrid vehicle shown in FIG. 18, the sun gear S1, carrier C1 and ring gear R1 of the first planetary gear set 14 are respectively connected to the first electric motor MG1, engine 12 and second electric motor MG2, while the sun gear S2, carrier C2 and ring gear R2 of the second planetary gear set 16 are respectively connected to the second electric motor MG2 and output gear 30, and to the housing 26 through the brake BK. The sun gear S1 and the ring gear R2 are selectively connected to each other through the clutch CL. The ring gear R1 and the sun gear S2 are connected to each other. In the drive system 170 for the hybrid vehicle shown in FIG. 19, the sun gear S1, carrier C1 and ring gear R1 of the first planetary gear set 14 are respectively connected to the first electric motor MG1, output gear 30 and engine 12, while the sun gear S2, carrier C2 and ring gear R2 of the second planetary gear set 16 are respectively connected to the second electric motor MG2 and output gear 30, and to the housing 26 through the brake BK. The sun gear S1 and the ring gear R2 are selectively connected to each other through the clutch CL. The carriers C1 and C2 are connected to each other. In the drive system 180 for the hybrid vehicle shown in FIG. 20, the sun gear S1, carrier C1 and ring gear R1 of the first planetary gear set 14 are respectively connected to the first electric motor MG1, output gear 30 and engine 12, while the sun gear S2, carrier C2 and ring gear R2 of the second planetary gear set 16 are respectively connected to the second electric motor MG2, to the housing 26 through the brake BK, and to the output gear 30. The ring gear R1 and the carrier C2 are selectively connected to each other through the clutch CL. The carrier C1 and ring gear R2 are connected to each other.

The drive systems for the hybrid vehicle shown in FIGS. 18-20 are identical with each other in that each of these drive systems for the hybrid vehicle is provided with the first differential mechanism in the form of the first planetary gear set 14 and the second differential mechanism in the form of the second planetary gear set 16, 16', which have four rotary elements (whose relative rotating speeds are represented) in

the collinear chart, and is further provided with the first electric motor MG1, second electric motor MG2, engine 12 and output rotary member (output gear 30) which are connected to the respective four rotary elements, and wherein one of the four rotary elements is constituted by the rotary element of the first planetary gear set 14 and the rotary element of the second planetary gear set 16, 16' which are selectively connected to each other through the clutch CL, and the rotary element of the second planetary gear set 16, 16' selectively connected to the rotary element of the first planetary gear set 14 through the clutch CL is selectively fixed to the housing 26 as the stationary member through the brake BK, as in the drive system for the hybrid vehicle shown in FIGS. 4-7. Namely, the hybrid vehicle drive control device of the present invention described above by reference to FIG. 8 and the other figures is suitably applicable to the drive systems shown in FIGS. 18-20.

As described above, the illustrated embodiments are configured such that the hybrid vehicle is provided with: the first differential mechanism in the form of the first planetary gear set 14 and the second differential mechanism in the form of the second planetary gear set 16, 16' which have the four rotary elements as a whole when the clutch CL is placed in the engaged state (and thus the first planetary gear set 14 and the second planetary gear set 16, 16' are represented as the four rotary elements in the collinear charts such as FIGS. 4-7); and the engine 12, the first electric motor MG1, the second electric motor MG2 and the output rotary member in the form of the output gear 30 which are respectively connected to the four rotary elements. One of the four rotary elements is constituted by the rotary element of the above-described first differential mechanism and the rotary element of the above-described second differential mechanism which are selectively connected to each other through the clutch CL, and one of the rotary elements of the first and second differential mechanisms which are selectively connected to each other through the clutch CL is selectively fixed to the stationary member in the form of the housing 26 through the brake BK. The drive control device is configured to start the engine 12 with the output torque of the second electric motor MG2, when a reaction force is exerted on the first and second electric motors MG1 and MG2. Accordingly, the engine 12 can be adequately started by cranking of the engine 12 with the second electric motor MG2, even in the event of a failure of the first electric motor MG1. Namely, the illustrated embodiments provide the drive control device in the form of the electronic control device 40 for the hybrid vehicle, which permits adequate starting of the engine 12.

The engine 12 is started with the output torque of at least one of the first and second electric motors MG1 and MG2, in the engaged state of the clutch CL and in the released state of the brake BK. For example, the engine 12 is cranked with both of the first and second electric motors MG1 and MG2, so that the rotary motion speed of the engine can be rapidly raised through a resonance band of the power transmitting system, whereby a starting shock of the engine 12 can be reduced.

The engine 12 is started primarily with the output torque of the second electric motor MG2, in the engaged state of the clutch CL and in the released state of the brake BK, in the event of a failure of the first electric motor MG1. Accordingly, the engine 12 can be adequately started by cranking with the second electric motor MG2, even in the event of a failure of the first electric motor MG1.

The engine 12 is started by bringing the clutch CL into the engaged state after a rise of the speed  $N_{MG2}$  of the second electric motor MG2 placed in the freely rotatable state, when either of the first and second electric motors MG1 and MG2 cannot generate the torque required to crank the engine 12.

Accordingly, the engine 12 can be adequately started by cranking the engine 12 by the output torque of the second electric motor MG2 having a rotary motion inertia, even where the output torque of the second electric motor MG2 should be limited due to excessive reduction of the electric energy amount SOC stored in the battery.

The engine 12 is started by bringing the clutch CL into the engaged state after the rise of the speed  $N_{MG2}$  of the second electric motor MG2 to the predetermined value  $N_{b_0}$  corresponding to the inertia force required to crank the engine 12. Accordingly, it is possible to crank the engine 12 in a highly practical manner for starting the engine 12, with the output torque of the second electric motor MG2 having the rotary motion inertia.

The first planetary gear set 14 is provided with a first rotary element in the form of the sun gear S1 connected to the first electric motor MG1, a second rotary element in the form of the carrier C1 connected to the engine 12, and a third rotary element in the form of the ring gear R1 connected to the output gear 30, while the second planetary gear set 16 (16') is provided with a first rotary element in the form of the sun gear S2 (S2') connected to the second electric motor MG2, a second rotary element in the form of the carrier C2 (C2'), and a third rotary element in the form of the ring gear R2 (R2'), one of the carrier C2 (C2') and the ring gear R2 (R2') being connected to the ring gear R1 of the first planetary gear set 14. The clutch CL is configured to selectively connect the carrier C1 of the first planetary gear set 14 and the other of the carrier C2 (C2') and the ring gear R2 (R2') which is not connected to the ring gear R1, to each other, while the brake BK is configured to selectively fix the other of the carrier C2 (C2') and the ring gear R2 (R2') which is not connected to the ring gear R1, to a stationary member in the form of the housing 26. Accordingly, it is possible to adequately start the engine 12 in the drive systems 10, etc., which have highly practical arrangements.

While the preferred embodiments of this invention have been described by reference to the drawings, it is to be understood that the invention is not limited to the details of the illustrated embodiments, but may be embodied with various changes which may occur without departing from the spirit of the invention.

---

#### NOMENCLATURE OF REFERENCE SIGNS

---

10, 100, 110, 120, 130, 140, 150, 160, 170, 180:	Hybrid vehicle drive system
12:	Engine 14: First planetary gear set (First differential mechanism)
16, 16':	Second planetary gear set (Second differential mechanism)
18, 22:	Stator 20, 24: Rotor 26: Housing (Stationary member)
28:	Input shaft 30: Output gear (Output rotary member)
32:	Oil pump 40: Electronic control device (Drive control device)
42:	Accelerator pedal operation amount sensor 44: Engine speed sensor
46:	MG1 speed sensor 48: MG2 speed sensor 50: Output speed sensor
52:	MG1 temperature sensor 53: MG2 temperature sensor
54:	Battery SOC sensor 56: Engine control device 58: Inverter
60:	Hydraulic control unit
70:	Engine starting requirement determining portion
72:	Clutch engagement control portion
74:	Brake engagement control portion
76:	Electric motor operation control portion
78:	MG1 failure determining portion
80:	Torque limitation determining portion
82:	MG2 speed determining portion
BK:	Brake CL: Clutch C1, C2, C2': Carrier (Second rotary element)
MG1:	First electric motor MG2: Second electric motor
OWC:	One-way clutch P1, P2, P2': Pinion gear
R1, R2, R2':	Ring gear (Third rotary element)
S1, S2, S2':	Sun gear (First rotary element)

---

The invention claimed is:

1. A drive control device for a hybrid vehicle provided with: a differential device which includes a first differential mechanism and a second differential mechanism and which has four rotary elements; and an engine, a first electric motor, a second electric motor and an output rotary member which are respectively connected to said four rotary elements, and wherein one of said four rotary elements is constituted by a rotary component of said first differential mechanism and a rotary component of said second differential mechanism which are selectively connected to each other through a clutch, and one of the rotary components of said first and second differential mechanisms which are selectively connected to each other through said clutch is selectively fixed to a stationary member through a brake, said drive control device comprising:

an electric motor operation control portion configured to control said second electric motor for starting said engine with an output torque of said second electric motor, when a reaction force is exerted on said first and second electric motors.

2. The drive control device according to claim 1, wherein said electric motor operation control portion controls said first and second electric motors to start said engine primarily with an output torque of said second electric motor, or output torques of said first and second electric motors, in an engaged state of said clutch and in a released state of said brake.

3. The drive control device according to claim 1, wherein said electric motor operation control portion controls said second electric motor to start said engine primarily with the output torque of said second electric motor, in an engaged state of said clutch and in a released state of said brake, in the event of a failure of said first electric motor.

4. The drive control device according to claim 1, wherein said electric motor operation control portion controls said

second electric motor to start said engine by bringing said clutch into an engaged state after a rise of a speed of said second electric motor placed in a freely rotatable state, when either of said first and second electric motors cannot generate a torque required to crank said engine.

5. The drive control device according to claim 4, wherein said electric motor operation control portion controls said second electric motor to start said engine by bringing said clutch into the engaged state after the rise of the speed of said second electric motor to a predetermined value corresponding to an inertia force required to crank said engine.

6. The drive control device according to claim 1, wherein said first differential mechanism is provided with a first rotary element connected to said first electric motor, a second rotary element connected to said engine, and a third rotary element connected to said output rotary member, while said second differential mechanism is provided with a first rotary element connected to said second electric motor, a second rotary element, and a third rotary element, one of the second and third rotary elements of the second differential mechanism being connected to the third rotary element of said first differential mechanism,

and wherein said clutch is configured to selectively connect the second rotary element of said first differential mechanism, and the other of the second and third rotary elements of said second differential mechanism which is not connected to the third rotary element of said first differential mechanism, to each other, while said brake is configured to selectively fix the other of the second and third rotary elements of said second differential mechanism which is not connected to the third rotary element of said first differential mechanism, to the stationary member.

\* \* \* \* \*